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(19) (CA) **CANADIAN PATENT** (12)

(54) Nickel Containing Catalysts

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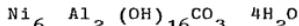
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This invention relates to a nickel containing catalyst composition of high thermal stability and which has outstanding resistance to carbon deposition, and is particularly but not exclusively for use in the steam reforming of hydrocarbons.

Nickel catalysts formed from coprecipitated materials and homogeneous on a microscopic scale are commonly used for the production of SNG by the low temperature steam reforming of liquid hydrocarbons. Similar materials may be used for the methanation of carbon oxides. These processes require catalysts of high activity at relatively low temperatures. Normally, the thermal stability and other physical parameters such as mechanical strength, and abrasion resistance of such catalysts are of secondary importance. The more successful catalysts are derived from a coprecipitated layer compound with the typical formulation.



This compound is formed from a solution of nickel and aluminium salts by the addition of alkali (for example, sodium carbonate), and is followed by calcination of the product in air and forming into a suitable shape by, for example, tabletting, to give the finished product. The



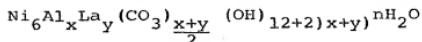
catalyst is normally reduced in situ prior to use.

Precipitation of the layer compound may also be brought about homogeneously using a hydrolysable organic material. Alkali metal oxides, in particular, potassium oxide may be included in the catalyst formulation to improve the carbon gasification activity of the reduced catalyst. More recent developments include a thermally stable material prepared in the same way but promoted by chromia, added in the form of chromium nitrate during the preparation.

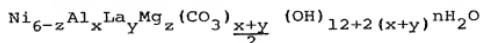
The present invention generally provides a method of making a catalyst said method being selected from the group of methods consisting of

(a) a method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium, lanthanum and if desired magnesium from a solution of their nitrates by addition of alkali, and recovering the precipitate characterized in that the pH and temperature of the solution are kept substantially constant throughout the reaction so that the precursor formed comprises a layer structure and has either

(i) the approximate chemical composition



or (ii) the approximate chemical composition



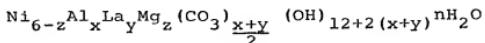
in which x is not less than 1 and not greater than 4;
y is not less than 0.05 and not greater than 1.5,
n is approximately 4 and z is in the range of from
0.1 to 4,

and

(b) a method of making a catalyst located in a porous body, comprising forming a catalyst precursor and then calcining the precursor characterized by forming a solution of salts of nickel, aluminium and lanthanum, adding a hydrolysable material to the solution, locating the combined solution within the pores of a preformed low surface area ceramic matrix, heating the combined solution to a temperature suitable for controlled hydrolysis of the hydrolysable material thereby increasing the pH to precipitate the nickel, aluminium and lanthanum salts within the pores whereby the catalytically active metal component is almost exclusively confined to the pores, and decomposing the metal salts to metal oxide or hydroxide form by calcining.

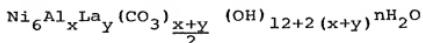
In accordance with an aspect of the present invention, there is provided a method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium, lanthanum and magnesium from a solution of their nitrates by addition of alkali, and recovering the precipitate characterized in that the pH and temperature of the solution are kept substantially

constant throughout the reaction so that the precursor formed comprises a layer structure and has the approximate chemical composition



in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4, and z is in the range of from 0.1 to 4.

In accordance with further particular aspect the present invention provides a method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium and lanthanum from a solution of their nitrates by addition of alkali, and recovering the precipitate characterized in that the pH and temperature of the solution are kept substantially constant throughout the reaction so that the precursor formed comprises a layer structure and has the approximate chemical composition



in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, and n is approximately 4.

In accordance with the present invention the pH of the solution may be kept at approximately 7. The solution may also be kept at room temperature.

In accordance with the present invention the precursor may be filtered from the solution in which it is precipitated, washed and dried and partially calcined at approximately 300°C before it is fully calcined.

In accordance with the method of the present invention the precursor may be of the defined formula where x is in the range of from 1.5 to 3 and y is in the range of from 0.1 to 0.5. The precursor may include one or more anions other than carbonate. The other anions may be selected for example from the group of anions consisting of a nitrate anion and a phosphate anion.

In accordance with the method of the present invention the catalyst precursor may be present in the pores of a pre-formed low surface area ceramic matrix.

In accordance with the method of the present invention the lanthanum component may be derived from pure lanthanum salts, or mixtures of rare earth salts. The rare earth salts may, for example, be lanthanum and cerium mixtures in which lanthanum is the major component.

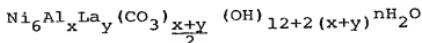
In accordance with the method of the present invention the precursor may include zirconium.

In accordance with an additional aspect the present invention in particular provides a method of making a catalyst located in a porous body, comprising forming a catalyst precursor and then calcining the precursor characterized by forming a solution of salts of nickel, aluminium and lanthanum, adding a hydrolysable material to the solution, locating the combined

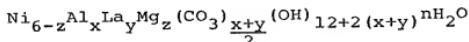
solution within the pores of a preformed low surface area ceramic matrix, heating the combined solution to a temperature suitable for controlled hydrolysis of the hydrolysable material thereby increasing the pH to precipitate the nickel, aluminium and lanthanum salts within the pores whereby the catalytically active metal component is almost exclusively confined to the pores, and decomposing the metal salts to metal oxide or hydroxide form by calcining. The ceramic matrix may have been pre-treated with alkali or acid to modify the interaction between the catalytically active material and the ceramic matrix. The surface of the ceramic matrix may have been modified by the addition of alumina spacer material within the pores of the ceramic matrix prior to the addition of the active phase.

In a further general aspect the present invention provides a catalyst derived from a precursor comprising nickel, aluminium and lanthanum, the precursor being adapted for calcining to form the catalyst characterized in that the precursor has a layer structure and is either

(i) of the approximate chemical composition



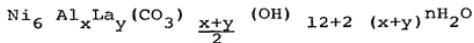
or (ii) of the approximate chemical composition



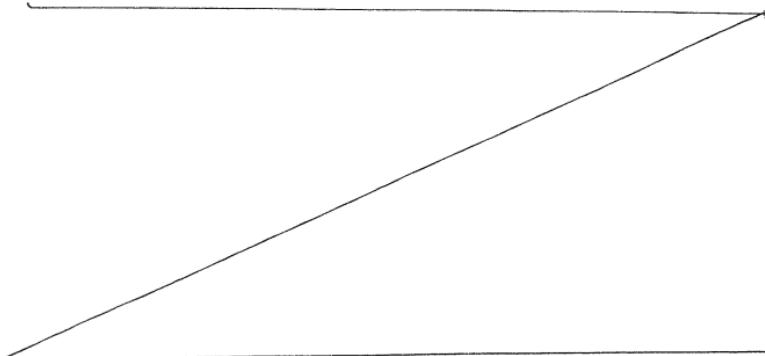
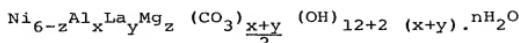
in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4, and z is in the range from 0.1 to 4. The catalyst

precursor may be present in the pores of a preformed low area ceramic matrix.

As indicated above according to the present invention, a catalyst is derived from a precursor of approximate chemical composition.



where x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5 and n is approximately 4. Preferably, x and y are in the range 1.5 to 3 and 0.1 to 0.5 respectively. It is possible for part of the nickel content to be replaced by magnesium. Therefore in accordance with a further aspect of the invention a catalyst is derived from a precursor of the approximate chemical composition.



and where z is not less than 0.1 and not greater than 4. Again it is preferred that x and y are in the range 1.5 to 3 and 0.1 to 0.5 respectively. In a preparative route based on coprecipitation lanthanum ions are incorporated in a layer structure. It is however not essential that lanthanum ions are so incorporated in a layer structure to realise the advantages of the overall catalyst composition of the invention. In the precursor, anions other than carbonate for example nitrates, phosphates etc., may also be present. The material may be prepared by coprecipitation from, for example, a solution of the nitrates, under controlled conditions of pH and temperature, by the addition of alkalis such as sodium carbonate, sodium hydroxide, ammonium bicarbonate or ammonium hydroxide. Preferably ammonium bicarbonate is used, as it has been found that the presence of sodium, even in trace amounts, has a detrimental effect on the activity and stability of the catalysts. Coprecipitation may also be induced by a homogeneous precipitation technique using a readily hydrolysable material such as urea. After precipitation, the material is filtered, washed and dried at elevated temperatures. It has been found that the removal of impurities such as

sodium ions may be facilitated if the material is dried at an elevated temperature prior to washing. The washed and dried material is preferably only partially calcined at a temperature of approximately 300° C prior to forming into a suitable shape for process requirements.

To achieve the overall catalyst composition of the invention it is obvious that other preparative techniques can be used such as sequential precipitation of each component or post-impregnation of the nickel-aluminium or nickel-aluminium-magnesium materials as the precipitate or the calcinate with a soluble salt of lanthanum. In either case the resultant material is subsequently dried, calcined and formed into a suitable shape.

The catalyst composition herein disclosed therefore relates to the addition of a lanthanum species to enhance the thermal stability and carbon gasification activity of a nickel containing material. The catalyst composition may be utilized either in a form in which it is held within a porous ceramic matrix or as an apparently homogeneous material, the form being chosen to meet the requirements of the particular process. The lanthanum component may be derived from pure lanthanum salts or mixtures of rare earth salts

particularly lanthanum and cerium mixtures in which lanthanum is the major component.

Nickel catalyst compositions containing a lanthanum species may be used for example in the high temperature steam reforming of hydrocarbons. Other possible applications include the methanation of gases containing high concentrations of carbon oxides particularly arising from coal gasification processes. Hitherto commercial catalysts for the high temperature steam reforming of hydrocarbons have been prepared either by impregnation of a preformed support or by co-forming the ingredients to give the required final shape. However, a process to improve the thermal stability and activity of catalysts under severe operating conditions has been described in copending Canadian patent application 395.860, in which an active material of high surface area is deposited within the pores of a preformed ceramic matrix by homogeneous precipitation techniques. The method allows the facile inclusion of various promoters and/or spacers. In this case the lanthanum species is preferably present in the precipitation solutions. However the lanthanum species may be added by post impregnation of the calcined nickel-aluminium material or nickel-aluminium-magnesium

material contained within the pores of the ceramic matrix and subsequently calcining the resultant material. Simple impregnation of the preformed ceramic matrix with the soluble salts of nickel, lanthanum and for example aluminium and subsequent calcination to the oxides may also be used as a preparative technique. The metal loading of the catalyst may be increased by multi-impregnation/drying/calcination steps.

In the aforementioned preparative routes involving a ceramic matrix the final catalyst composition has the preferable range of nickel contents of 5-30 wt. % and 0.1-15 wt. % as lanthanum. If aluminium is present in the material added to the ceramic matrix it is preferred that the atomic ratios of Ni:Al in the active material are 1.5 to 4 : 1. If magnesium is present in the nickel-aluminium phase, it is preferred that the atomic ratios of Ni:Mg in the active material at 1 to 20:1.

Preferably the preformed ceramic matrix has an apparent porosity in the range 15% to 80% and has a mean pore diameter in the range 0.1 μ m to 20 μ m. In the special case of hollow shapes such as hollow spheres the porosity and mean pore diameter of the wall will be in the aforementioned range. The preformed ceramic matrix may be ~~ox~~-alumina but

other preformed matrixes of ceramic materials such as silicon carbide aluminosilicates, silica etc., may be used.

The ceramic matrix may be pretreated with acid or alkali to modify the interaction of the catalytically active material and the ceramic matrix. The surface of the ceramic matrix may also be modified by the addition of "spacer/support" material, for example, alumina within the pores of the ceramic matrix prior to the addition of the active phase. This may be accomplished by the simple impregnation of the ceramic matrix with a soluble salts of the "spacer/support" material e.g. aluminium nitrate or by using the homogeneous precipitation technique. In each case the temperature of the calcination of the impregnated ceramic matrix must be carefully controlled to achieve the required surface properties.

In the preferred preparation of the lanthanum containing catalyst composition for high temperature applications, the preformed α -alumina matrix is impregnated, under vacuum with a solution containing nickel, lanthanum and aluminium nitrates and also a precipitation agent such as urea. It should be noted that other promoters/spacers such

as zirconium may be added, preferably as the nitrate, to further increase the stability and/or improve the selectivity of the catalyst. After draining, the ~~an~~- alumina matrix may be heated to a temperature suitable for the controlled hydrolysis of the urea thus increasing the H of the absorbed solution and bringing about the deposition of the insoluble hydroxides within the pores. The catalyst is then dried by heating to a suitably elevated temperature.

The metal loading of the catalyst may be increased by repetition of the process steps. Prior to re-impregnation of the catalyst the pores must be opened. In one aspect of the process the pores may be opened by thermal decomposition of material within the pores. Alternatively the catalyst is washed with water or weaker alkaline solution and then dried at a suitably elevated temperature. The catalyst of the required metal loading is subjected to a final calcination temperature of about 450° C.

Several non-limiting examples of the process of the invention and catalysts produced thereby are given below.

Example 1

Coprecipitated Samples A and B were prepared using the following procedures.

A solution A was prepared by dissolving 291g of $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, 150g of $\text{Al}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ and 32g of $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ in 1dm³ of de-ionised water; solution B was prepared by dissolving 300 g of anhydrous ammonium bicarbonate in 2.5dm³ of de-ionised water. Solution A was added dropwise and with vigorous stirring to solution B, both being maintained at room temperature. The pH remained at approximately 7 throughout the addition. When this was complete, the resultant slurry was heated slowly and with vigorous stirring to 80°C to complete the precipitation by ensuring that any soluble nickel bicarbonate formed at 20°C was decomposed. The precipitate was then filtered to dryness in a Buchner funnel, dried at 100°C in a ventilated oven for 48h, washed in boiling de-ionised water (4dm³), and refiltered in the Buchner funnel where it was further washed with five idm³ portions of boiling de-ionised water. It was then redried at 100°C in the ventilated oven for 24h. The resultant material was ground to a fine powder and a sample of it was transferred to a silica boat in a tubular furnace in which it was heated in a flow of pure argon over a period of 175 min from

room temperature to 450°C, at which temperature it was maintained for 17h. This process brought about the complete decomposition of the precipitate to a mixture of the oxides. (Calcination in air rather than treatment in argon is also possible). -The furnace was then cooled to 200°C and hydrogen was mixed with the argon so that the H₂:Ar ratio was 2.0. The temperature was raised from 200°C to 600°C over a period of 170 min and the temperature was then maintained at 600°C for 2h. This brought about reduction of the nickel component of the catalyst. The temperature was lowered to room temperature and the sample was passivated by turning off the hydrogen flow and diverting the argon through a bottle containing water prior to contacting the catalyst, for a period of 3h, with the argon + water mixture. The catalyst so produced had a Ni/Al atomic ratio of 2.5 and the lanthanum content, expressed as an atomic fraction ($\frac{La}{Ni+Al+La}$) was 0.05. The catalyst was designated Sample A.

An equivalent material (Sample B) was prepared following an identical procedure but omitting the lanthanum nitrate from Solution A, all other components being the same.

The Ni particle diameters of Samples A and

B were determined by X-ray diffraction line-broadening techniques and were found to be 165 Å and 156 Å respectively. The samples were then aged in H₂/H₂O flows (H₂/H₂O = 8) at 800°C for a period of 3h, a test which is generally accepted to give an indication of the stability of the supplies. It was found that in both cases, the resultant particle size was approximately 400 Å.

Thus, we conclude that the presence of lanthanum has no detrimental effect on the resistance to sintering of the coprecipitated catalysts, each sintering to approximately the same extent.

The activities of samples A and B for the methanation of carbon monoxide were tested using a differential scanning calorimeter before and after the sintering test referred to above. It was found that the activity of sample A at 300°C was 74% of the fresh activity after the sintering test while that of sample B was 88% of the fresh activity after the test. We therefore conclude that lanthanum imparts a slight advantage to the catalyst in preserving its activity after exposure to H₂/H₂O atmospheres. The catalysts so produced have good thermal stability and are capable of resisting carbon laydown.

Example 2

A quantity of the washed precipitate from which was prepared Sample B was immersed in a solution of $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ the quantity and strength of the solution being such that the precipitate was just wetted and the quantity of lanthanum so introduced into the catalyst was such that the atomic fraction ($\frac{\text{La}}{\text{Ni} + \text{Al} + \text{La}}$) was 0.012. The sample was then decomposed and reduced as described in Example 1 (designated Sample C) and was tested for methanation activity in the DSC. The activity of Sample C at 300°C was 54% higher than that of sample A.

Example 3

100g of a pure $\alpha\text{-Al}_2\text{O}_3$ which had been formed in the shape of Raschig rings (6mm x 6mm) and having a total surface area of $0.7\text{m}^2\text{g}^{-1}$ and having a water absorption of 30% and a mean pore diameter of approximately 2.5 m were vacuum impregnated with a solution of 350g of $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ and 73g of urea dissolved in 150cm³ of deionised water. Excess of the solution was drained from the $\alpha\text{-Al}_2\text{O}_3$ matrix. The impregnated rings were laid in a single layer on an aluminium tray and were placed in a ventilated oven at 95°C for 17h. Hydrolysis of the urea took place and a precipitate formed in

the pores of the matrix. Decomposition of the precipitate and reduction of the resultant NiO was carried out as in Example 1 except that the decomposition was 4h and reduction time (at 600°C) was 4h. The sample, designated Sample D, was passivated as before. A higher metal loading of the sample could be achieved by further impregnating the rings after thermal decomposition at 310°C in an air oven for 2h, a procedure which was essential to open the pores of the rings for further absorption of solutions.

Further samples were prepared using a solution of 350g $(\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, 150g $\text{Al}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ and 217g urea in 150g of deionised water, and using a similar solution containing 50.5g of $\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ in addition to the Ni and Al salts and the urea. Both samples were decomposed and reduced as for Sample D and were designated Samples E and F respectively. As for Sample D, the metals content could be increased by a series of steps involving partial decomposition and further impregnation. The following table gives the Ni contents (wt.%) of the reduced samples, the Ni particle diameters determined by X-ray diffraction and the total surface area (determined by adsorption of Krypton at -195°C):

Sample	Ni content /wt.%	Average Ni particle diameter/ \AA	Total surface Area/ m^2g^{-1}
D	4.5	257	2.5
E	4.3	198	7.6
F	4.2	117	6.5

It can be seen that the presence of Al gives an improved dispersion of the nickel and that La gives an even greater improvement. The increase in surface area compared with that of the $\alpha\text{-Al}_2\text{O}_3$ matrix ($0.7\text{m}^2\text{g}^{-1}$) also reflects these improvements in dispersion.

Example 4

The samples D, E, and F prepared in Example 3 were tested in a tubular flow reactor for their activities in the low pressure steam reforming of a heptane feed at an exit temperature of 650°C . The steam:carbon ratio was 4:1. Sample D was found to have good activity initially but this decreased with time and after 1h, the sample had disintegrated presumably due to the deposition of carbon in the voids of the matrix. Sample E gave an improved activity but, although it did not disintegrate, back-pressure built up, again presumably due to carbon deposition. Sample F gave 100% conversion of the heptane feed over the period of the test and there was no evidence for carbon

deposition. We therefore conclude that, in the α - Al_2O_3 matrix, La has an advantageous effect on the catalyst, preventing carbon deposition reactions (i.e. giving greater carbon gasification rates).

Example 5

Catalyst samples D, E and F were compared for their methanation activities in the differential scanning calorimeter. Their activities at 300°C were in the ratio 6:3:2. It was noted that sample D became deactivated when methanation was carried out above 450°C. The samples were also subjected to a steam sinter test as described in Example 1, the duration of the test being 4h. The subsequent activities of the samples were in the ratio 1:10:18. We therefore conclude that La improves the stability of the Ni-Al formulation when held in the α - Al_2O_3 matrix much more than it does the coprecipitate (see Example 1).

Example 6

The precursor to Sample F was washed using a series of different reagents prior to the decomposition stage. The reagents used were water, NaOH (0.1M), Na_2CO_3 (0.1M), $(\text{NH}_4)_2\text{CO}_3$ (0.1M) and KOH(0.1M). Samples of the undecomposed material were immersed in these reagents which has been

preheated to 80-90°C and the temperature was raised to the boiling point of the reagent for 10 min. The reagent was then decanted and replaced by two portions of deionised water. In all cases, a volume of reagent three times that of the sample was used. The samples were then dried in a ventilated oven at 120°C for 17h. Thermal analysis investigations showed that water, KOH and NaOH were most effective at removing unreacted nitrates and unhydrolysed urea from the $\alpha\text{-Al}_2\text{O}_3$ matrix, leaving behind pure precipitates as described above. The washed samples were heated in argon to decompose the precipitate and reduced as described in Example 3. Their relative activities at 300°C for the methanation of CO were determined with the differential scanning calorimeter as follows:

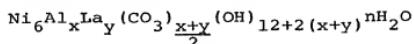
Sample F	Ni content after washing /wt %	Relative activity at 300°C
NO treatment	5.4	1.0
H_2O	3.9	2.6
NaOH	5.1	2.5
Na_2CO_3	4.5	1.0
$(\text{NH}_4)_2\text{CO}_3$	5.1	1.4
KOH	not determined	2.8

Example 7

Two samples equivalent to samples E and F were made by a series of three depositions as described above. The La-free sample had a Ni content of 10.4 wt % and the La-containing sample had a Ni content of 9.5 wt %. The Ni areas of the samples were found, using hydrogen chemisorption at 20°C, to be 0.4 and 0.96 m²g⁻¹ respectively. This further demonstrates the effect of La on the active material held within the α -Al²O₃ matrix, the Ni area being proportioned to the activity of the catalyst.

The embodiments of the invention in which an exclusive property or privilege is claimed are defined as follows:

1. A method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium and lanthanum from a solution of their nitrates by addition of alkali, and recovering the precipitate characterised in that the pH and temperature of the solution are kept substantially constant throughout the reaction so that the precursor formed comprises a layer structure and has the approximate chemical composition



in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, and n is approximately 4.

2. A method according to claim 1, characterised in that the pH of the solution is kept at approximately 7.

3. A method according to claim 1, characterised in that the solution is kept at room temperature.

4. A method according to claim 2, characterised in that the solution is kept at room temperature.

5. A method according to claim 1, 2 or 3, characterised in that the precursor is filtered from the solution in which it is precipitated, washed and dried and partially calcined at approximately 300°C before it is fully calcined.

6. A method according to claim 4, characterised in that the precursor is filtered from the solution in which it is precipitated, washed and dried and partially calcined at approximately 300°C before it is fully calcined.

7. A method according to claim 1, 2 or 3, characterised in that the precursor is of the defined formula where x is in the range of from 1.5 to 3 and y is in the range of from 0.1 to 0.5.

8. A method according to claim 6, characterised in that the precursor is of the defined formula where x is in the range of from 1.5 to 3 and y is in the range of from 0.1 to 0.5.

9. A method according to claim 1, 2 or 3, characterised in that the precursor includes one or more anions other than carbonate.

10. A method according to claim 8, characterised in that the precursor includes one or more anions other than carbonate.

11. A method according to claim 10, wherein said anions are selected from the group of anions consisting of a nitrate anion and a phosphate anion.

12. A method according to claim 1, 2 or 3, characterised in that the catalyst precursor is present in the pores of a preformed low surface area ceramic matrix.

13. A method according to claim 8, characterised in that the catalyst precursor is present in the pores of a preformed low surface area ceramic matrix.

14. A method according to claim 1, 2 or 3, characterised in that the lanthanum component is derived from pure lanthanum salts, or mixtures of rare earth salts.

15. A method according to claim 13, characterised in that the lanthanum component is derived from pure lanthanum salts, or mixtures of rare earth salts.

16. A method according to claim 15, characterised in that the rare earth salts are lanthanum and cerium mixtures in which lanthanum is the major component.

17. A method according to claim 1, 2 or 3, characterised in that the precursor includes zirconium.

18. A method according to claim 8, characterised in that the precursor includes zirconium.

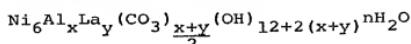
19. A method of making a catalyst located in a porous body, comprising forming a catalyst precursor and then calcining the precursor characterised by forming a solution of salts of nickel, aluminium and lanthanum, adding a hydrolysable material to the solution, locating the combined solution within the pores of a preformed low surface area ceramic matrix, heating the combined solution to a temperature suitable for controlled hydrolysis of the hydrolysable material thereby increasing the pH to precipitate the nickel, aluminium and lanthanum salts within the pores whereby the catalytically active metal component is almost exclusively confined to the pores, and decomposing the metal salts to metal oxide or hydroxide form by calcining.

20. A method according to claim 19, characterised in that the ceramic matrix has been pre-treated with

alkali or acid to modify the interaction between the catalytically active material and the ceramic matrix.

21. A method according to claim 19, characterised in the surface of the ceramic matrix has been modified by the addition of alumina spacer material within the pores of the ceramic matrix prior to the addition of the active phase.

22. A catalyst derived from a precursor comprising nickel, aluminium and lanthanum, the precursor being adapted for calcining to form the catalyst characterised in that the precursor has a layer structure and is of the approximate chemical composition



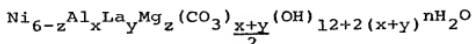
in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5 and n is approximately 4.

23. A catalyst according to claim 22, characterised in that x is in the range of from 1.5 to 3 and y is in the range of from 0.1 to 0.5.

24. A catalyst according to claim 22 or 23, characterised in that the catalyst precursor is present in the pores of a preformed low area ceramic matrix.

25. A method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium, lanthanum and magnesium from a solution of their nitrates by addition of alkali, and recovering the precipitate char-

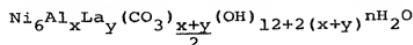
acterised in that the pH and temperature of the solution are kept substantially constant throughout the reaction so that the precursor formed comprises a layer structure and has the approximate chemical composition



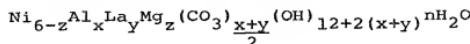
in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4, and z is in the range of from 0.1 to 4.

26. A method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium, lanthanum and if desired magnesium from a solution of their nitrates by addition of alkali, and recovering the precipitate characterised in that the pH and temperature of the solution are kept substantially constant throughout the reaction so that the precursor formed comprises a layer structure and has either

(i) the approximate chemical composition



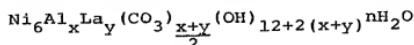
or (ii) the approximate chemical composition



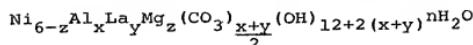
in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4 and z is in the range of from 0.1 to 4.

27. A catalyst derived from a precursor comprising nickel, aluminium and lanthanum, the precursor being adapted for calcining to form the catalyst characterised in

that the precursor has a layer structure and is either
 (i) of the approximate chemical composition

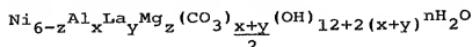


or (ii) of the approximate chemical composition



in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4, and z is in the range from 0.1 to 4.

28. A catalyst derived from a precursor comprising nickel, aluminium and lanthanum, the precursor being adapted for calcining to form the catalyst characterised in that the precursor has a layer structure and is of the approximate chemical composition



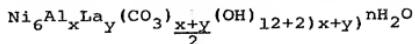
in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4 and z is in the range from 0.1 to 4.

29. A method of making a catalyst said method being selected from the group of methods consisting of

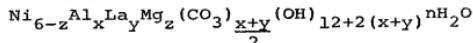
- (a) a method of forming a catalyst comprising nickel, aluminium and lanthanum, by first forming a catalyst precursor and then calcining the precursor, the precursor being formed by co-precipitating nickel, aluminium, lanthanum and if desired magnesium from a solution of their nitrates by addition of alkali, and recovering the precipitate characterised in that the pH and temperature of the solution are kept substantially constant throughout the reaction so that the precursor formed comprises a layer structure

and has either

(i) the approximate chemical composition



or (ii) the approximate chemical composition



in which x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5, n is approximately 4 and z is in the range of from 0.1 to 4,

and

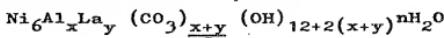
- (b) a method of making a catalyst located in a porous body, comprising forming a catalyst precursor and then calcining the precursor characterised by forming a solution of salts of nickel, aluminium and lanthanum, adding a hydrolysable material to the solution, locating the combined solution within the pores of a preformed low surface area ceramic matrix, heating the combined solution to a temperature suitable for controlled hydrolysis of the hydrolysable material thereby increasing the pH to precipitate the nickel, aluminium and lanthanum salts within the pores whereby the catalytically active metal component is almost exclusively confined to the pores, and decomposing the metal salts to metal oxide or hydroxide form by calcining.

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ABSTRACT

"Catalyst"

The invention relates to a nickel containing catalyst composition of high thermal stability and which has outstanding resistance to carbon deposition, and is particularly but not exclusively for use in the steam reforming of hydrocarbons. Nickel catalysts formed from coprecipitated materials and homogeneous on a microscopic scale are commonly used for the production of SNG by the low temperature steam reforming of liquid hydrocarbons. Similar materials may be used for the methanation of carbon oxides. These processes require catalysts of high activity at relatively low temperatures. Normally, the thermal stability and other physical parameters such as mechanical strength, and abrasion resistance of such catalysts are of secondary importance. The object of the invention is to provide an improved catalyst, which object is met by a catalyst derived from a precursor of approximate chemical composition



where x is not less than 1 and not greater than 4; y is not less than 0.05 and not greater than 1.5 and n is approximately 4.

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